

Total gas in-place calculations for the Baltic-Podlasie-Lublin basin shales in Poland

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Abstract. The total gas in-place calculations reflecting Polish reservoir conditions were performed using a corrected version for the free gas in-place, where not only the pore conditions were taken under consideration but also the volume that was already occupied by the sorbed gas. Shales show very different capacities between samples mainly due to in-situ conditions.

1 Introduction

During the first decade of XXI century and, to the lesser degree, also Canada experienced “energetic revolution” related to production of unconventional resources of gas and oil. A significant impact on gas and oil prices as well as in energy security was achieved due to the fast increase of production of these resources. Technologic and economic success of this sector of petroleum industry in North America has inspired attempts to export this concept to other continents, including Europe, at the beginning of the second decade of XXI century. Most intensive exploration of shale gas and oil, apart from US and Canada, took place in the Lower Paleozoic Baltic-Podlasie-Lublin Basin in Poland [1,2].

According to the International Energy Agency, Poland has become one of the countries with potentially the largest shale gas deposits. An accurate assessment of these deposits is a key factor to allow Poland to reduce the foreign dependency of this gas from Russia and other former Soviet republics [3, 4].

2 Methodology

In order to estimate the total gas in-place, equation 1 is used.

$$G_{st} = G_a + G_f \quad (1)$$

This equation is divided in volumetric and surface components. In this equation G_{st} is the total gas in-place, G_f is the volumetric component involving hydrocarbons stored in the pore space as free gas, and G_a is the surface component, with the gas physically adsorbed on the large surface area of the micropores [5].

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The surface component is calculated using equation:

$$G_a = G_L \cdot \frac{p}{p+p_L} \quad (2)$$

where G_L is the Langmuir volume, p is the pressure and p_L is the Langmuir pressure. Equation 3 is used to calculate the volumetric component,

$$G_f = \frac{32,0368}{B_g} \left[\frac{\phi(1-S_w)}{\rho_b} - \frac{1,318 \times 10^{-6} M}{\rho_s} \left(G_L \frac{p}{p+p_L} \right) \right] \quad (3)$$

where B_g is the gas formation volume factor, ϕ is the porosity of the rock, S_w the water saturation, M the molar mass, ρ_b the bulk rock density and ρ_s the sorbed phase density.

This model takes under consideration, not only the adsorbed gas, but also the free gas stored inside the pores to give a more accurate value of the total gas in-place. It is particularly important that, unlike in coals, the ratio of adsorbed gas-to-free gas is much lower. For calculation of the total free gas in-place, the adsorbed gas must be calculated and subtracted from this calculation and corrected for the water saturation [5]. This methodology may give a new overview on the comprehensive assessment of CH₄ potential of Polish shales as a strategic reservoir for CH₄.

3 Calculations and results

Two samples were tested with completely different parameters as shown in Table 1. Sorption measurements were performed using the high precision manometric sorption setup, located in the Institute of Mining at the Silesian University of Technology (Figure 1.) Calculations of the sorption capacities and Langmuir models are shown in Fig. 2.

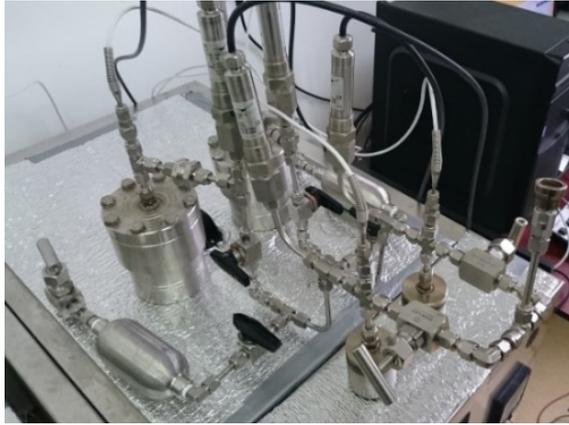


Figure 1. High precision manometric setup at the Silesian University of Technology, Poland.

Parameters related to the in-situ conditions of the basin were supplied by the drilling company and some of them are shown in Table 1.

Taking under consideration the in-situ characteristics of the basin and the tests performed in the laboratory both components of Equation (1) were calculated. The surface component, dependent on the sorption capacities, and thus on the rock composition, showed proportional values to the sorption capacities calculated with 2.06 sm³/t for sample no. 1 and 3.37 sm³/t for sample no. 2. The volumetric component mostly depended on the porosity and water saturation of the samples. It greatly impacted the results obtained for sample no. 1 with only 0.12 sm³/t of free gas, while sample no. 2 had 3.92 sm³/t of free gas. These results are shown in Figure 3 for comparison.

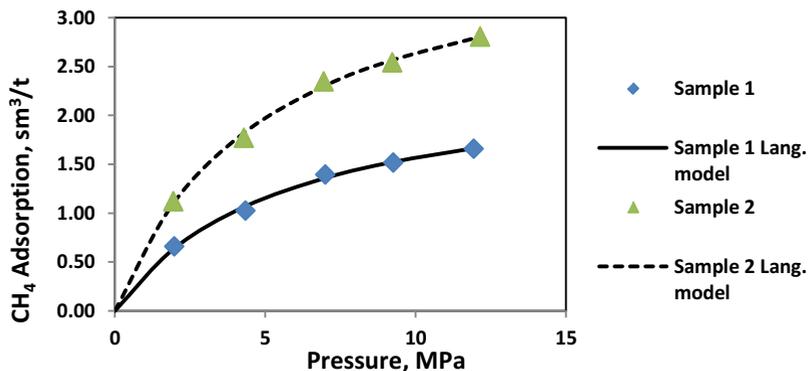


Figure 2. Methane sorption measurements and Langmuir model for Polish shales.

Table 1. Some of the in-situ parameters of the samples.

	Sample 1	Sample 2
Porosity, %	5.16	9.50
Water saturation, %	70.61	35.00
Bulk rock density, g/cm ³	2.67	2.40
Total Organic Carbon, %	1.25	4.19

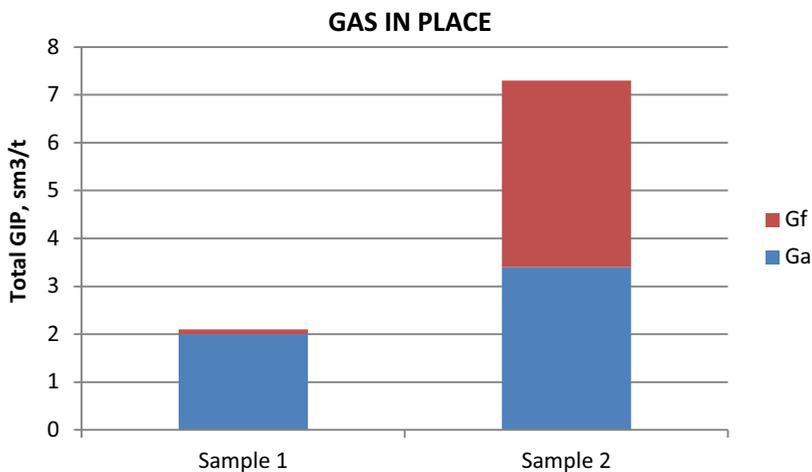


Figure 3. Results obtained in the total gas-in-place calculations.

4 Results and conclusions

Results obtained in the study showed that the biggest impact while calculation of the total GIP, was not produced by the rock composition, but by the basin conditions. Thus, a sample that during a preliminary analysis may seem to be the worse choice due to its composition, could be as good as

higher organic matter sample under the adequate conditions. In the data exposed, it can be observed that sample no. 2 is better than sample no. 1, related to the surface component, by a 70%. However when taking under consideration the free gas, this value increases up to 250%,

To get a better idea of this, we decided to apply the basin data from sample no. 2 to the sample no. 1, with a hypothetical result of gas-in-place of $6.7 \text{ sm}^3/\text{t}$. These new values are shown in Figure 4. With these suppositions, the total gas in place difference, due to the rock composition, is reduced.

For the correct understanding of the data, the subtracting factor from Equation 3 has to be taken under consideration. The higher the sorption capacity, the lower total free gas calculation. It is due to the volume of pore that is taken by the sorbed gas on the surface of pores.

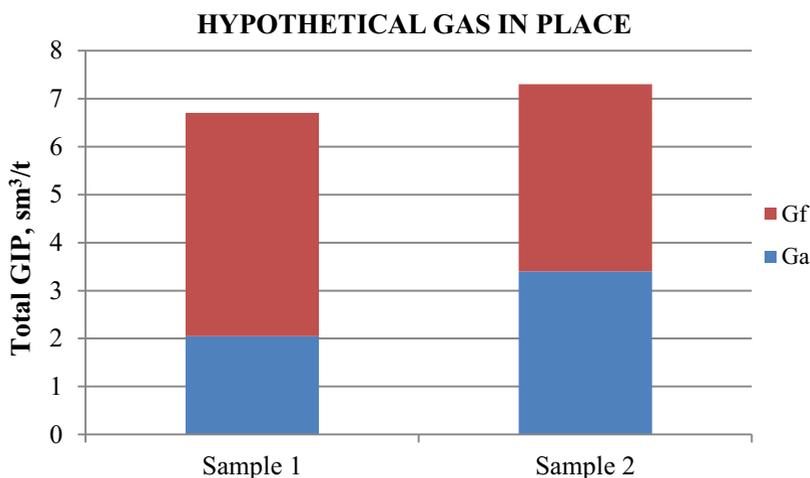


Figure 4. Hypothetical results obtained using the same main parameters for both samples.

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