Reference P-wave velocity in coal seams at great depths in Jastrzebie coal mine

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Abstract. In the study, the determining of the reference velocity of the P-wave in coal seams used in seismic profiling to assess increases and decreases in relative stresses at large depths has been presented. The seismic profiling method proposed by Dubinski in 1989 covers a range of depth up to 970 m. At present, coal seams exploitation in Polish coal mines is conducted at greater depths, even exceeding 1200 m, which creates the necessity for a new reference velocity model. The study presents an empirical mathematical model of the change of the P-wave velocity in coal seams in the geological conditions of the Jastrzebie coal mine. A power model analogous to the Dubinski's one was elaborated with new constants. The calculations included the results from 35 measurements of seismic profiling carried out in various coal seams of the Jastrzebie mine at depths from 640 to 1200 m. The results obtained cause changes in the result of calculations of seismic anomalies. Future validation of the proposed model with larger data set will be required.

Key words: rock burst hazard, Dubinski method, seismic profiling, refracted P-wave

1 Introduction

In Polish hard coal mines, the Dubinski's seismic profiling method [1-2] is often used to assess the rock burst hazard. This method is based on measurement of the refracted P-wave velocity in the coal seam. The measured velocity changes depend on the stress-strain state, which has a significant impact on the rock burst hazard [3-5].

Seismic anomaly is calculated as a ratio of measured P-wave velocities to the so-called reference velocity for depth of the survey. This velocity was statistically calculated based on the results of several hundred seismic measurements in depth range 190 - 970 m [1]. Due to the development of coal seam exploitation at ever greater depths, even exceeding 1200 m, and an increasing threat of the rock bursts [6], there is a need to verify the formula of the reference velocity as a function of depth.

The seismic profiling method was used to solve many research tasks related to the exploitation of coal seams in rock burst hazard conditions. Tor et al. [7] presented an example of using the method to assess the effectiveness of destressing blasting in the Jas-Mos hard

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coal mine. Research has allowed to identify zones requiring implementation of preventive measures.

Seismic profiling was conducted for the use of the damping factor as an additional seismic parameter [8-11]. Pilecki and Klosinski [8] came to the conclusion that the damping factor is more sensitive to the changes of stress in the rock mass compared to indication based on velocity of the P-wave. This result was confirmed by Wojtecki and Dzik [11].

Interesting study was conducted by Olechowski et al. [12] who compared the results of seismic profiling with the results of the WAS-96/RMS method [13]. They concluded that the seismic profiling method provides more reliable results. In addition, seismic profiling results are continuous as opposed to discrete results of the WAS-96/RMS method. It should be emphasized, however, that the WAS-96/RMS method is very useful in assessing rock burst hazard in a heading face zone.

Szreder and Barnas [14] reported that “*seismic profiling in underground excavations was also carried out for different purposes in other geological conditions for example: in a salt body to estimate the width of the fracture zone in the side-walls of excavations [15] and also in tunneling [16-17]*”

The aim of this study is to modify the Dubinski's formula [1] for calculation the reference velocity of P-wave in coal seams for its applicability at greater depths below 1000 m in the geological conditions of Jastrzebie coal mine. The calculations of the modified formula took into account 35 new values of P-wave velocity measured at a depth of 900 to 1200 m. The introductory part of the article presents the theoretical foundations of the seismic profiling method. Then geological conditions in Jastrzebie coal mine have been described. The main part of the study presents the assumptions for calculating the reference velocity formula, the results of statistical calculations and their analysis. coal mine

2 Theoretical background of seismic profiling in coal seams

The velocity of refracted P-wave in coal seam is the basic parameter calculated from seismic profiling in Dubinski method [1]. This is the velocity of a wave propagating along an excavation in an elastic zone (not disturbed by excavation) on the border with a plastic zone (disturbed by excavation). The border between elastic and plastic zones may be illustrated by the use of a Ladanyi model (fig.1).

Fig. 1. Model of behaviour of a rock mass around an excavation ([9] on the basis of [18]) σ_1 - major principal stress, σ_3 - minor principal stress, σ_θ - tangential stress, σ_r - radial stress, ε_1 - major principal strain, p_0 - virgin stress, p_1 - lining load.

In practice, the interpretation of the refracted P-wave is not easy, because this border is transient. An additional problem is related to the fact that the velocity of the determined P-wave does not differ significantly from the velocity of the refracted S-wave in shale layers in the roof and the bottom of the coal seam (Fig. 2) [14]. At greater distances from the excitation

point, the first breaks of the refracted P-wave in shale layers overtakes or distorts the first breaks of the P-wave in the coal seam.

Fig. 2. Seismogram with selected P- waves, S-waves and the channel wave.

Comparison of the measured V_P velocity with the reference velocity V_0 for a given depth allows for calculation of the seismic anomaly according to the formula [2]:

$$A = \frac{V_P - V_0}{V_0} \cdot 100 \text{ [%]} \tag{1}$$

The calculated seismic anomaly (fig. 3) is used for assessment of probable increase or decrease in relative stress (tab. 1).

Fig. 3. An example of the results of seismic profiling at a depth of about 900 m in "Borynia-Zofiowka-Jastrzebie" Hard Coal Mine with the reference velocity V_0 (dashed line) and the anomaly A_1 marked [19].

The empirical formula for the reference velocity V_0 was determined on the basis of laboratory tests and several hundred seismic measurements carried out in the Upper Silesian Coal Basin hard coal mines (39 mines, 292 measurements) in 190-970 m depth range [1]:

$$V_0 = 1200 + 4.83h^{0.76}$$

(2)

where *h* is the depth of the measurement site.

Table 1. Seismic scale of relative stress changes in Upper Silesian Coal Basin conditions for depth range 500 – 900 m [2].

Degree of relative stress increase (decrease)	Positive (negative) seismic anomaly [%]	Scale of relative stress increase (decrease)	Probable increase (decrease) in relative stress [%]
0	< 5 (>-7.5)	Lack / very low	< 20 (<25)
1	5 – 15 (-7.5 ÷ -15)	Low	20 – 60 (25 ÷ 55)
2	15 – 25 (-15 ÷ -25)	Medium	60 – 140 (55 ÷ 80)
3	> 25 (< -25)	High	> 140 (>80)

3 Geological and mining conditions in the research area in Jastrzebie coal mine

The Jastrzebie coal mine is located in the southwestern part of the Upper Silesian Coal Basin east of the Orlowo overlap. The Jastrzebie mining area is bordered on the west by the Radlin mining area coinciding with the overlap border (disturbance) of the Orlowo-Boguszowice region, on the north by the Borynia mining area, on the east by the Zofiowka mining area, and on the south by the closed Moszczenica mining area (Fig. 4).

The main geological element in this area is the Jastrzebie anticline running from NE to SW, also called the Mszana-Jastrzebie saddle [20]. The coal deposit is dominated by folded tectonics. The faults located in the Jastrzebie coal mine area have small throws (up to 30 meters) [21].

The Jastrzebie mining area consists of Quaternary, Neogene (Miocene) and Upper Carboniferous (productive) formations. The top of Upper Carboniferous deposits in the Jastrzebie mining area lie directly under Neogene and Quaternary formations at a depth of 60 to 150 m [21]. They are represented by conglomerates, sandstones, mudstones and claystones with numerous hard coal seams of varying thickness from a few centimeters to about 9 meters. Carboniferous deposits are developed as Ruda beds (group 400), Saddle beds (group 500) and Poreba beds (group 600).

Seismic profiling measurements were carried out in coal seams located in Saddle beds. These beds consist mainly of sandstone formations. They also contain mudstones and claystones, which usually accompany coal seams. The thickness of the beds is 240-290 m. It was found that the 501, 502 and 503 coal seams are separated by 5-15 m sandstone layers, 504 coal seam (0.5-3 m) lies between sandstone and shales series and 505 and 506 (1.5-3.5m) coal seams are often combined. The 510 coal seam reaches the greatest thicknes of 4-5 m [21].

In the tested coal seams of saddle beds, the uniaxial compressive strength of coal Rc=4.2-19.4 MPa and bulk density γ₀=12.5-13.4 kN/m³ (MEERI PAS reports).

Fig. 4. Location of the Jastrzebie mining area (borders marked in blue), (source: Geoportal GeoLOG).

4 The reference velocity formula calculation methodology

In order to determine the modified Dubinski's formula [1], the following calculation methodology was used:

1. For reference velocity calculations, all archival values (246) from Dubinski's dataset [1] and additional values (35) measured by MEERI PAS team at depths 640-1200 m in coal seams: 505/2, 510/1, 510/1lg, 510/2, 510/2ld were used. The MEERI PAS team performed the research in the years 2006-2019. In total, 281 values were analyzed.
2. It was assumed that the reference velocity V_0 changes with the depth h according to the mathematical model determined by Dubinski [1]: $V_0 = 1200 + ah^b$.
3. Based on the regression analysis, only velocity values less than double the standard deviation σ were used for further calculations:

$$\sigma = \sqrt{\frac{\sum_{i=1}^n (y_i - \hat{y}_i)^2}{n}} \quad (3)$$

where: $\hat{y}_i$ - the theoretical values calculated from the regression model, y_i - the measured values and n - the number of measured values.

4. New coefficients were calculated for the power model $V_0 = 1200 + ah^b$ along with the error assessment based on the coefficient of determination R^2 :

$$R^2 = \frac{\sum_{i=1}^n (\hat{y}_i - \bar{y})^2}{\sum_{i=1}^n (y_i - \bar{y})^2} \quad (4)$$

where: $\bar{y}$ – arithmetic mean of empirical values of the explained variable.

The velocities from seismic profiling measurements were determined from the sections of the profile, the least disturbed by mining and geological factors, i.e. the influence of faults, longwall and heading faces, edges of adjacent, exploited seams and etc. Despite these efforts, the choice of measurement sites may influence on calculations of reference velocity.

5 The results of calculations and their analysis

Table 2 summarizes the information on the set of archival data [1] and new data obtained from seismic profiling in the Jastrzebie coal mine in the years 2006-2019.

Table 2. Characterization of the dataset used for calculations.

Parameter	Dataset	
	Jastrzebie dataset	Dubinski archival data
Number of velocity values	25	245
Coefficient of determination R^2	0.69	0.81
Minimum depth [m]	670	190
Maximum depth [m]	1200	970
Minimum P-wave velocity [m/s]	1900	1500
Maximum P-wave velocity [m/s]	2330	2200
Average P-wave velocity [m/s]	2095	1870

From all 281 velocity values, those that were greater than double the standard deviation ($\sigma=155$ m/s) were rejected. As a result, 25 velocity values from the Jastrzebie coal mine and 245 velocities from the archival collection were used for the calculations, which in total gave 270 values (Fig. 5).

The range of velocity values from the Jastrzebie coal mine is 1900-2330 m/s, with the average velocity of 2095 m/s and standard deviation 120 m/s, whereas the range of the archival dataset is 1500-2200 m/s, with the average velocity of 1870 m/s, and the standard deviation 134 m/s (Tab. 2). The dataset from Jastrzebie coal mine was characterized by noticeably higher velocity values compared to the archival dataset. This difference is related to the greater average depth of measurement in Jastrzebie coal mine, but also to the possible influence of various geological and mining factors.

The results of the regression analysis are presented in Table 3. As a result of the calculations for the conditions of Jastrzebie coal mine we propose the following modified Dubinski's formula:

$$V_0=1200+2.73h^{0.85} \quad (5)$$

The R^2 determination coefficient for the modified model was 0.82, while the standard deviation σ was equal to 63 m/s. Figure 6 presents Dubinski's general model and our formula for the conditions of Jastrzebie coal mine. Both models do not differ significantly. The Jastrzebie coal mine model is more similar to a linear model than the general model of Dubinski. In addition, the Jastrzebie coal mine plot is within the data range (200 - 1200 m) in the regression range of the linear plot for the 95% confidence interval. It was noticed that the linear model with the form $V_0=1300+0.88h$ has the same coefficient of determination (0.82) and standard deviation (63 m/s) as the power model of Jastrzebie coal mine.

The difference between Dubinski's formula and the new Jastrzebie coal mine formula is close to zero for a depth of 600 m, and then it increases with depth: for 900 m it has ~35 m/s and for 1200 m it has ~75 m/s.

It should be noted that the Jastrzebie coal mine formula still needs verification after collecting more data below a depth of about 1100 m.

Fig. 5. The plot of archival dataset (red points) and new dataset from Jastrzebie coal mine (blue points) together with the regression curve for all data (blue line) and the general Dubinski’s formula (dashed black line). Outliers are marked in yellow.

Table 3. Determination coefficients R^2 and standard deviation σ for the Dubinski’s formula and Jastrzebie coal mine formula.

Reference velocity model		Coefficient of determination R^2	Standard deviation σ
Dubinski’s formula (Archival dataset)	$V_0= 1200+4.83h^{0.76}$	0.77	64
Jastrzebie coal mine formula (Archival and Jastrzebie dataset)	$V_0=1200+2.73h^{0.85}$	0.82	63

Fig. 6. The plot of the Dubinski model, and the Jastrzebie coal mine power and linear model.

6 Resume

Dubinski's formula [1] for calculating the reference P-wave velocity in coal seams depending on the depth was determined for maximum depth of 970m. Currently, coal seams are mined at greater depths, even exceeding 1200 m. Therefore, there is a need to adapt this formula to greater depths. In the study we modified Dubinski's formula by taking into account additional 35 reference velocity values measured in the geological and mining conditions of the Jastrzebie coal mine within the depth range of 640-1200 m. Based on the calculations made, the following conclusions were drawn:

1. The dataset from Jastrzebie coal mine differs from the Dubinski's dataset for the depths below 900 m. P-wave velocities values are much higher than it would result from the Dubinski model. Therefore, an attempt to calculate the formula taking into account new dataset was found to be justified.
2. As a result of statistical calculations for the geological and mining conditions of Jastrzebie coal mine a power formula is proposed in the following form:

$$V_P = 1200 + 2.73h^{0.85}$$
3. After obtaining more data, especially from a depth below 1100 m, the formula should be recalculated.

References

1. J. Dubinski, *Sejsmiczna metoda wyprzedzającej oceny zagrożenia wstrzasami górnictwymi w kopalniach węgla kamiennego (Seismic method of shock hazard assessment in hard coal mines)*, Central Mining Institute (1989) (in Polish)
2. J. Dubinski, W. Konopko, *Tapania – ocena, prognoza, zwalczanie (Rock bursts – assessment, prognosis, defeating)* Wyd. GIG, Katowice (2000) (in Polish)
3. Z. Pilecki, *Dynamic analysis of mining tremor impact on excavation*, Proc. Int. FLAC Symp. on Numerical Modeling in Geomechanics, Detournay & Hart, 397–400 (1999)
4. J. Dubinski, Z. Pilecki, W. Zuberek, *Badania geofizyczne w kopalniach – przeszłość, teraźniejszość, i zamierzenia na przyszłość (Geophysical research in mines - past, present and future plans)*, MEERI PAS, Krakow (2001) (in Polish)
5. Z. Burtan, A. Zorychta, J. Cieslik, D. Chlebowski D., Arch Min Sci **59** (3) 691–704 (2014) doi: 10.2478/amsc-2014-0048
6. G. Mutke, J. Dubinski, A. Lurka *New criteria to assess seismic and rock burst hazard in coal mines*, Arch Min Sci **60** (3) 743–760 (2015) doi: 10.1515/amsc-2015-0049
7. A. Tor, P. Chmiel, Z. Pilecki, A. Jakubow, R. Skatula, Z. Szreder, J. Klosinski, *Kontrola efektywności strzelan torpedujących za pomocą profilowania sejsmicznego (Control of the effectiveness of torpedo blastings using seismic profiling)*, Bezpieczeństwo Pracy i Ochrona Środowiska w Górnictwie, Miesięcznik WUG **142** (6) 62–64 (2006) (in Polish)
8. Z. Pilecki, J. Klosinski, *Profilowanie tłumienia fali sejsmicznej w pokładzie węgla (Profiling of seismic wave attenuation in a coal seam)*, Bezp. Pracy i Ochrona Srod. w Górnictwie, Materiały Warsztatów, 381–393 (2007) (in Polish)
9. Z. Szreder, Z. Pilecki, J. Klosinski, *Efektywność rozpoznania oddziaływania krawędzi eksploatacyjnych metodami profilowania tłumienia oraz predkosci fali sejsmicznej (Effectiveness of recognition of the impact of exploitation edges by methods of seismic wave attenuation and velocity profiling)*, Gospod Surow Min **24** (2/3) (2008) (in Polish)
10. Z. Szreder, Z. Pilecki, J. Klosinski, *Comparison of Profiling Results of Attenuation and Velocity of Refracted P-wave in Coal-seam*, Proc. 14th EAGE European Meeting of Environmental and Engineering Geophysics (2008) doi: 10.3997/2214-4609.20146265
11. L. Wojtecki, G. Dzik, *Profilowanie sejsmiczne ociosów chodników węglowych w wersji kinematycznej i tłumieniowej (Seismic profiling along sidewalls in the kinematic and attenuation versions)* Mine Mechanization and Automation **50**(4) 29–37 (2012) (in Polish)
12. S. Olechowski, K. Krawiec, J. Kokowski, Z. Szreder, P. Harba, M. Cwiekala, *Comparison of the results of the seismic profiling and WAS-96/RMS seismoacoustic active method in an assessment of the impact of the overlying coal seam edge*, E3S Web Conf **66**, 01011 (2018) doi: 10.1051/e3sconf/20186601011
13. J. Kornowski, H. Sokolowski, M. Trombik, A. Wasko, *Zasady i zakres stosowania metody wzbudzonej aktywności sejsmoakustycznej WAS-96/RMS do oceny stanu zagrożenia tapaniami (The principles and scope of application of the method of induced seismoacoustic activity WAS-96/RMS for the assessment of rock bursts threat)* Central Mining Institute, Instrukcje 4, Katowice (1996) (in Polish)
14. Z. Szreder, M. Barnas, *Assessment of the impact of an overlying coal seam edge using seismic profiling of refracted P-wave velocity*, E3S Web Conf **24**, 01007 (2017) doi: 10.1051/e3sconf/20172401007
15. J. Slizowski, Z. Pilecki, K. Urbanczyk, E. Pilecka, L. Lankof, R. Czarny, Adv High Energy Phys, 1–12 (2013) doi: 10.1155/2013/461764

16. Z. Majcherczyk, Z. Pilecki, E. Niedbalski, E. Pilecka, M. Blajer, J. Pszonka, *Wpływ warunków geologiczno-inżynierskich i geotechnicznych na dobór parametrów obudowy wstępnej tunelu drogowego w Lalikach (Impact of geological, engineering and geotechnical conditions on the selection of parameters of the initial support of the road tunnel in Laliki)*, Gospod Surowcami Min **28** (1) 103–124 (2012) (in Polish)
17. M. Kudyk, Z. Pilecki, *Moduł deformacji utworów fliszu karpackiego na trasie tunelu "Emilia" w Beskidzie Żywieckim (Modulus of deformation of Carpathian flysch on the route of the "Emilia" tunnel in the Żywiec Beskids)*. Zeszyty Naukowe IGSMiE PAN **76**, 45–64 (2009) (in Polish).
18. B. Ladanyi, *Use of the long-term strength concept in the determination of ground pressure on tunnel linings*, Proc. of the 3rd Congress of the Int. Soc. for Rock Mech., II, B, 1150–1156, Denver (1974)
19. *Raport 2/2016, Wyniki profilowania sejsmicznego w rejonie chodnika nadścianowego 28a-C3 sciany 28b w pokładzie 510/1 w KWK „Borynia-Zofiówka-Jastrzebie” Ruch Jastrzebie (Report 1/2019 Results of seismic profiling in the gallery 28a-C3 of longwall 28b in the 510/1 coal seam in KWK "Borynia-Zofiówka-Jastrzebie" Ruch Jastrzebie)* IGSMiE PAN Krakow, (2019) (in Polish)
20. J. Gustkiewicz (red.), *Właściwości fizyczne skal karbońskich górnosląskiego zagłębia węglowego. Skaly warstw siodłowych (Physical properties of Carboniferous rocks of the Upper Silesian coal basin. Rocks of Saddle beds)*, Wyd. IGSMiE PAN Krakow (1999) (in Polish)
21. W. Gabzdyl, *Charakterystyka petrograficzno-facjalna pokładów węgla i skal towarzyszących w Kopalni Jastrzebie (Rybnicki Okręg Węglowy) (Petrographic and facial characteristics of coal seams and associated rocks in the Jastrzebie coal mine (Rybnik Coal Area))*, Wydawnictwa Geologiczne (1969) (in Polish)