Comparative Study on Flow Characteristics of Pipeline System Based on CFD

Hou Yingzhe 1, Wu Hao 1, Yan Xiaozhe 1, Zhu Haoqiang 1, Gao Haitao 1, Hu Yiming 1, Cui Qiguan 1, Xiong Jinying 1, Zhou Longyu 1

Wuhan Secondary Ship Design and Research Institute, Wuhan, Hubei, 430205, China

Abstract. Based on the CFD numerical simulation method, this paper established a pipeline model to study the internal flow characteristics of three different combinations of hot water pipeline systems and thus obtained the flow field information such as pressure, flow rate, and flow rate inside the pipeline. The study results showed that the smoother the pipeline transition, the smaller the velocity uniformity coefficient; the higher the uniformity of the flow field, the smaller the pressure and velocity fluctuations, the smaller the resulting pipeline vibration. Besides, the flow characteristics have been greatly improved.

1 INTRODUCTION

The hot water pipeline system is widely used in energy, shipbuilding, petrochemical, machinery, and other industries. It is the bridge and link connecting boilers, heat accumulators, heat exchangers, and other equipment in the power system. If the pipeline's design and layout are unreasonable, its resistance loss will be too large or too small. Too much resistance will cause the medium to flow poorly, and too small resistance will cause the medium to flow excessively and fastly, thus causing the pipeline to vibrate and affect the system's safety and reliability. Meanwhile, there are many pipelines, a variety of specifications, and complex arrangements in a large pipeline network. However, the pipeline network's arrangement and direction have significant limitations due to the limited space. Therefore, the pipeline network design should not only complete the arrangement of the pipeline system in the limited space, but also ensure that the parameters of each piece of equipment can reach the requirements of stable operation during running.

This paper studied the flow characteristics of the valve test system matched with the action performance test and discharge test of the regulator safety valve, analyzed three different pipeline combinations to improve the flow characteristics, and proposed an optimization scheme of the pipeline system combination.

2 STRUCTURE PRINCIPLE AND PERFORMANCE PARAMETERS

2.1. Structure principle

The hot water test circuit is mainly composed of a 19 m³ heat accumulator, a 5 m³ hot water container, valves, pipelines, and accessories, as shown in Fig. 1.

2.2 Performance Parameters

Parameters of Hot Water Pipeline System (Table 1):

<table>
<thead>
<tr>
<th>Description</th>
<th>Value</th>
</tr>
</thead>
<tbody>
<tr>
<td>Heat accumulator volume</td>
<td>19 m³</td>
</tr>
<tr>
<td>Hot water container volume</td>
<td>5 m³</td>
</tr>
<tr>
<td>Maximum test pressure (MPa)</td>
<td>20</td>
</tr>
</tbody>
</table>

Corresponding author: 15172526878@163.com

© The Authors, published by EDP Sciences. This is an open access article distributed under the terms of the Creative Commons Attribution License 4.0 (http://creativecommons.org/licenses/by/4.0/).
<table>
<thead>
<tr>
<th>Temperature Range (℃)</th>
<th>333~343</th>
</tr>
</thead>
<tbody>
<tr>
<td><strong>Medium</strong></td>
<td>Saturated/supercooled water</td>
</tr>
<tr>
<td>Heat accumulator outlet line</td>
<td>φ406×25</td>
</tr>
<tr>
<td>Connecting lines</td>
<td>φ273×34/φ406×25/φ406×50</td>
</tr>
<tr>
<td>Hot water container inlet line</td>
<td>φ273×34</td>
</tr>
</tbody>
</table>

In this paper, a comparative analysis is carried out on the specifications of two connecting pipelines in the pipeline system from a 19 m³ heat accumulator to a 5 m³ hot water container. The specific system pipeline combination is as follows:

1) Scheme A:
- Heat accumulator outlet line φ 406 × 25
- Connecting lines φ 273 × 34
- Hot water container inlet line φ 273 × 34

2) Scheme B:
- Heat accumulator outlet line φ 406 × 25
- Connecting lines φ 406 × 25
- Hot water container inlet line φ 273 × 34

3) Scheme C:
- Heat accumulator outlet line φ 406 × 25
- Connecting lines φ 406 × 50
- Hot water container inlet line φ 273 × 34

### 3 Numerical Simulation

#### 3.1. Governing equation

Captions should be typed in 9-point Times. They should be centred above the tables and flush left beneath the figures.

In this paper, the mature standard model was used for numerical simulation, and the governing equations were composed of continuity equation, momentum conservation equation, turbulent kinetic energy $\kappa$ equation, and dissipation energy equation.

**Continuity equation**

$$ \frac{\partial \rho_i}{\partial t} + \frac{\partial }{\partial x_j} (\rho_i u_j) = 0 $$

(1)

**Momentum conservation equation (N-S equation) formula**

$$ \rho \frac{d u_i}{d t} = \frac{\partial }{\partial x_j} \left[ \mu \left( \frac{\partial u_i}{\partial x_j} + \frac{\partial u_j}{\partial x_i} - \frac{2}{3} \delta_{ij} \frac{\partial u_k}{\partial x_k} \right) \right] $$

+ $$ \frac{\partial }{\partial x_j} (-\mu_i u_i) $$

(2)

The transport equations $\varepsilon$ of turbulent kinetic energy $k$ and turbulent kinetic energy dissipation rate of the standard turbulence model can be expressed as:

$$ \frac{\partial (\rho k)}{\partial t} + \frac{\partial (\rho k u_j)}{\partial x_j} = \frac{\partial }{\partial x_i} \left[ \mu \left( \frac{\partial }{\partial x_j} \right) \frac{\partial k}{\partial x_i} \right] + P - \rho \varepsilon $$

(3)

Where $u_i$ - the velocity component in the direction $i$, $i=1, 2, 3$

$\mu$ - Kinematic viscosity coefficient of the medium

$\varepsilon_i$ - Eddy viscosity coefficient

$\delta_k$ - Prandtl number corresponding to turbulent kinetic energy $k$

$\delta_\varepsilon$ - Prandtl number corresponding to turbulent kinetic energy dissipation rate $\varepsilon$

$P$ - turbulent kinetic energy generation term

$$ P = \mu_i \left( \frac{\partial u_i}{\partial x_j} + \frac{\partial u_j}{\partial x_i} \right) \frac{\partial u_i}{\partial x_j} $$

(5)

wherein:

$$ \mu_i = C_\mu \rho \frac{k^2}{\varepsilon} $$

(6)

$k$-$\varepsilon$ Empirical constants in the model (Table 2):

<table>
<thead>
<tr>
<th>$C_{\varepsilon_1}$</th>
<th>$C_{\varepsilon_2}$</th>
<th>$C_\mu$</th>
<th>$\delta_k$</th>
<th>$\delta_\varepsilon$</th>
</tr>
</thead>
<tbody>
<tr>
<td>1.44</td>
<td>1.92</td>
<td>0.09</td>
<td>1.0</td>
<td>1.3</td>
</tr>
</tbody>
</table>

#### 3.2 Establishment of Flow Channel Model and Meshing

According to the specific structure parameters, the 3D model of the pipeline system is established by CATIA software, and the internal flow channel model is generated by reverse modeling of fluid mechanics software. The flow channel model is imported into ANSYS ICEM CFD for meshing (Fig. 2). The mesh for numerical calculation is divided by tetrahedral/hybrid mesh, and the flow channel corners are locally encrypted to make the calculation results more accurate, and the mesh independence test is performed.
Combined with the running state of the hot water pipeline system in actual working conditions, the internal flow model under typical working conditions is established. The 3D incompressible flow Reynolds time-averaged equations and k-ε turbulence model are used to form a closed equation set to solve the internal flow field of the pipeline system. The fluid medium is set to water, and the temperature change is not considered during the solution process. The heat accumulator outlet is set as the pressure inlet boundary condition, with a velocity of 19.5 MPa. The inlet 1 and 2 of the hot water container are set as the pressure outlet boundary condition of 17.2 MPa. The pipe wall is set as the adiabatic non-slip boundary condition, and the 3D flow field is numerically simulated and analyzed.

4 Study on Internal Flow Characteristics

4.1 Pressure Field Distribution

Fig. 3 is a pressure nephogram of different pipeline combinations. As shown from the figure, Scheme A’s pressure gradient changes significantly, with uneven pressure distribution and a maximum pressure appearance at the end of the pipeline. That of Scheme B is small, with a smooth transition of pressure fluctuation and relatively uniform distribution. Compared with Schemes A and B, Scheme C has the smoothest pressure fluctuation and the most optimized flow characteristics.

4.2 Velocity field distribution

A velocity distribution nephogram is obtained after study on the velocity field distribution of different pipeline combinations, as shown in Fig. 4. As shown from the figure, Scheme A’s flow rate is relatively high, with significant velocity gradient changes and maximum velocity appearance at the junction of the outlet pipeline of the heat accumulator and the connecting pipeline, causing certain scouring to the pipeline. Scheme B’s maximum flow rate is generated at the hot water container inlet, with a relatively gentle velocity fluctuation and a low flow rate area formed at the connecting pipeline compared with other schemes. Compared with Schemes A and B, Scheme C gradually changes in transition, with uniform velocity distribution, stable tends, and optimized flow characteristics.
c) Scheme C

![Velocity Vectors Colored By Velocity Magnitude(m/s)](attachment:image)

**Figure 4.** Velocity Nephogram of Different Pipeline Combinations

### 5 Conclusion

1. Scheme C adopts φ 406 × 50 connecting pipelines, and the variation law of pressure gradient and velocity gradient tends to be more stable than Schemes A and B.
2. The smoother the pipeline combination transition, the higher the uniformity of the flow field, the smaller the pressure and velocity fluctuations, the smaller the pipeline vibration, and the flow characteristics will be greatly improved.

### References