Composite polypropylene polymer materials that work in contact with raw cotton

Olim Eshkobilov¹*, and Giyas Gulyamov²

¹Karshi Engineering-Economic Institute, Karshi, Uzbekistan
²State Unitary Enterprise “Fan va tarakkiyot” at Tashkent state technical university named after Islom Karimov, Tashkent, Uzbekistan

Abstract. Physicomechanical and tribotechnical properties of structural composite materials based on thermoplastic polymer and organomineral ingredients operating under friction and wear conditions during contact with pulp (raw cotton) have been investigated. The regularities of changes in the physical, mechanical and tribotechnical properties of structural composite materials during contact interaction with raw cotton were determined, the dependence of their properties on the type and content of graphite, mineral and fibrous fillers in structural composite materials was studied. It has been established that the nature and structure of fillers has a certain effect on the physical and mechanical properties of composite materials based on polypropylene. At the same time, fiber-filled compositions have the highest mechanical strength. It was also found that when mineral fillers are introduced into composite polymer materials, their coefficient of friction with raw cotton increases significantly, while the wear rate decreases, except for fillers with a plate structure (kaolin, talc), when used, a decrease in the coefficient of friction is observed. The introduction of carbon-graphite fillers into the composition of composite materials leads to a significant decrease in the coefficient of friction, temperature and static electricity charge in the friction zone with raw cotton. The introduction of fillers with a fibrous structure leads to a significant decrease in the rate of wear of the composites. It provides high strength and resistance of the material under thermomechanical action. Effective compositions of structural composite materials for work under conditions of contact interaction with fibrous mass have been developed, and their physical, mechanical and tribotechnical properties have been investigated.

1 Introduction

At present, the intensification of the development of cotton growing is of great importance, especially in mechanization and processing of raw cotton, which occupies a special place in the economy of Uzbekistan. Increasing the efficiency of cotton growing can be achieved through the comprehensive mechanization of all processes, from harvesting to cotton processing, increasing the efficiency and productivity of the machines and mechanisms.

*Corresponding author: polegon11@mail.ru

© The Authors, published by EDP Sciences. This is an open access article distributed under the terms of the Creative Commons Attribution License 4.0 (http://creativecommons.org/licenses/by/4.0/).
used while maintaining the natural indicators of raw cotton. One of the directions for solving the problem is developing new effective structural composite polymer materials and their use in cotton machines and mechanisms.

The details of the working bodies of cotton machines are operated under difficult loading conditions when interacting with raw cotton in compacted riots. Structural composite polymer materials increase their performance and ensure minimal damage to cotton fiber while maintaining its natural properties. Also, the development and use of new structural composite polymeric materials provide an increase in the productivity of machines, a decrease in power consumption, and excludes the possibility of cotton ignition and fiber winding on the surface of the peg parts.

In most of the well-known works, the development of antifriction-wear-resistant composite polymer materials was carried out without taking into account studies of the influence of the nature, type, content of polymer and fillers in composites, and these works did not investigate the processes of temperature change and the formation of static electricity during contact interaction in systems "polymer-cotton" and "composite-cotton", which made it impossible to obtain materials with a low coefficient of friction and high wear resistance.

Based on the molecular-mechanical theory of friction, a molecular-mechano-electrical theory was developed that describes the processes occurring during the contact interaction of a material with a fibrous mass.

The aim of this work is to study the physical, mechanical and tribotechnical properties (friction coefficient, wear rate, temperature and static electricity charge in the friction zone) of new structural composite materials with antifriction properties and high wear resistance based on a thermoplastic polymer and organomineral fillers for operation under conditions contact interaction with pulp-raw cotton.

2 Materials and Methods

We investigated structural composite materials based on thermoplastic polymer-polypropylene (TU 6-05-1105-80) grade 05P10/020 - with mineral (ground talc - GOST 879-52, kaolin - GOST 6138-81, wollastonite, chalk - GOST 17498-85), fibrous (fiberglass - TU6-11-191-90, cotton lint - GOST 9849-74) and carbon-graphite (graphite - GOST 5261-85, soot - TU 5-52 ATG-70) fillers. These fillers differ in shape and particle size: granular (soot), lamellar and flaky (graphite, kaolin, talc, wollastonite), fibrous (fiberglass, cotton lint). The average particle size of the filler should be between 1-50 microns.

The choice of fillers is due to the following:
- graphite and carbon black improve the thermal and electro-physical properties of the composite;
- fiberglass and cotton lint give the high strength material and increase resistance to thermomechanical effects due to reinforcement;
- talc, kaolin, chalk and wollastonite are available and inexpensive compared to other materials, which makes it possible to reduce the cost of structural composite materials with a polyolefin matrix.

To study the antifriction properties and wear resistance of polymer compositions operating under friction conditions, raw cotton of the 1st grade of a manual collection with a moisture content of 8-20%, contamination of 1-3% at an average density was used as a counterbody laying 170-180 kg/m³ (50-70 kg/m³ - loosened free-lying raw cotton, 240-250 kg/m³ packed raw cotton). Such values of moisture and contamination of raw cotton are the most typical for the operation of the harvesting network of the cotton gin industry.

The method of obtaining structural composite materials and manufacturing samples was as follows. Composite materials were obtained by mixing organomineral fillers in a mixer
with a movable cup, which was then mixed with a polymer binder in a two-chamber mixer with electric heating. The grinding was carried out after their preliminary mixing in a given proportion on a dismembrator unit, the principle of operation of which is based on impact-splitting and abrasion effects. The rotation speed of the working body of the dismembrator was 1500 rot./min.

Material with a particle size of up to 15 mm was continuously poured into the hopper of a working dispenser, from where it fell into a hollow tube and was pre-crushed under the impact of a rotating shaft. In this case, the material continuously moved in the direction of the stationary and rotating discs, in the zone of which it is crushed.

The physical and mechanical properties of structural composite materials were studied using generally accepted standard methods, and the complex of tribotechnical properties in interaction with raw cotton was studied on a disk tribometer.

### 3 Results and Discussion

As a result of the studies carried out, the effect of carbon-graphite, mineral and fibrous fillers on the physical, mechanical and tribotechnical properties of polypropylene under conditions of contact interaction with raw cotton was studied. The breaking stress (σₘ) and modulus of elasticity (E) in bending, hardness (HB) and impact strength (σᵢₛᵢ). This is because the efficiency and durability of composite polymer pegs of working bodies of cotton machines and mechanisms are mainly determined by these indicators of the splitting material and the tribotechnical properties during friction with raw cotton. As is known, σₘ - characterizes the resistance of a material to fracture at sufficiently high deformation rates; E - is a characteristic necessary in assessing the strength of a material and determines the nature of the contact frictional interaction and the actual contact area (ACA) during elastic contact of rubbing surfaces; σᵢₛᵢ - is one of the main characteristics of the material that determines the structural strength; HB is an important characteristic of the material that determines the ACA in plastic contacting.

Figures 1-8 show the results of a study of the physical-mechanical and tribotechnical properties of structural composite materials based on polypropylene, depending on the type and content of mineral, fibrous and carbon-graphite fillers.

As can be seen from Fig. 1, the introduction of mineral, fibrous and carbon-graphite fillers - fiberglass, cotton lint, wollastonite, and chalk up to 20-30 m.p. including leads to an increase in the breaking stress during bending of composite polypropylene materials (CPPM) to a maximum.
Fig. 1. Dependences of the breaking stress in bending of CPPM on the type and content of mineral, fibrous and carbon-graphite fillers.

A further increase in the content of these fillers is accompanied by a gradual decrease in the values of the breaking stress in bending. With the introduction of such mineral ingredients as talc, kaolin and, especially, carbon-graphite fillers - soot and graphite in polypropylene, the breaking stress during bending decreases with an increase in their content.

However, the magnitude of the breaking stress in bending remains rather high for compositions filled up to 15-20 m.p. including talc, kaolin and up to 5-10 m.p. including soot and graphite.

In general, the increase in flexural strength up to a certain filler content appears to be related to its accumulation in the interspherolite regions, where the filler enters during crystallization. The decrease in the strength of the compositions at high fillings is apparently caused by the fact that the presence of a large amount of filler between the polymer macromolecules somewhat complicates the energy of their intermolecular interaction, accelerating the process of decomposition of the composition.

The impact strength of CPPM with an increase in fibreglass content, lint and wollastonite up to 30 m.p., cement up to 10-15 m.p. also increases and then decreases. With the introduction of other fillers, the impact strength value gradually decreases with increased filler content (Figure 2).
Fig. 1. Dependences of the breaking stress in bending of CPPM on the type and content of mineral, fibrous and carbon-graphite fillers.

A further increase in the content of these fillers is accompanied by a gradual decrease in the values of the breaking stress in bending. With the introduction of such mineral ingredients as talc, kaolin and, especially, carbon-graphite fillers - soot and graphite in polypropylene, the breaking stress during bending decreases with an increase in their content.

However, the magnitude of the breaking stress in bending remains rather high for compositions filled up to 15-20 m.p. including talc, kaolin and up to 5-10 m.p. including soot and graphite.

In general, the increase in flexural strength up to a certain filler content appears to be related to its accumulation in the interspherolite regions, where the filler enters during crystallization. The decrease in the strength of the compositions at high fillings is apparently caused by the fact that the presence of a large amount of filler between the polymer macromolecules somewhat complicates the energy of their intermolecular interaction, accelerating the process of decomposition of the composition.

The impact strength of CPPM with an increase in fibreglass content, lint and wollastonite up to 30 m.p., cement up to 10-15 m.p. also increases and then decreases. With the introduction of other fillers, the impact strength value gradually decreases with increased filler content (Figure 2).

Fig. 2. Dependences of the impact strength of CPPM on the type and content of fillers.

The hardness of CPPM (Fig. 3) with the introduction of fiberglass, lint, cement, kaolin is up to 30 m.p., talc, soot and graphite up to 10-15 m.p. increases and then decreases.

The flexural modulus of CPPM (Fig. 4) gradually increases with an increase in the content of mineral fillers.

Fig. 3. Dependences of Brinell hardness of CPPM on the type and content of fillers

Fig. 4. Dependences of the elastic modulus in bending of CPPM on the type and content of fillers.

Comparing the results of measurements of the main indicators of the strength of CPPM shows that the values of the breaking stress in bending, impact toughness, hardness and elastic modulus in bending depend on the type and content of mineral, fibrous and carbon-
graphite fillers. In this case, the greatest strength is possessed by a polypropylene composition filled with 30-40 m.p., including fiberglass. For example, when adding fillers of fiberglass, talc, soot, graphite, kaolin, chalk, wollastonite and cotton lint up to 10 m.p.

Such an increase in the flexural strength and impact toughness of the polypropylene composition filled with fiberglass and cotton lint is explained by the reinforcing ability of the fiber filler and the high strength of fiberglass. A decrease in properties when the content is more than 30 m.p., including fiberglass and cotton lint, is explained by the lack of wetting of the fibrous fillers by the polymer matrix. In places where the fillers are not wetted, air bubbles appear, which are local points of concentration of internal stresses in the matrix, i.e. centres of the destruction of the polymer composition.

The addition of talc to polypropylene insignificantly changes the flexural strength of composite materials. This is due to the scaly shape of this filler and its high specific surface area.

It is known that the filling of polymers with carbon black leads to an increase in the rigidity of the material and the modulus of elasticity; therefore, this leads to a decrease in the toughness of the composition. The results of the experimental data confirm this position.

In general, the decrease in the strength of CPPMs at high fillings is apparently caused by the acceleration of the processes of destruction of the polymer composition. Dangerous defects appear in composite materials.

A change in the hardness value with a low content of mineral, fibrous and carbon-graphite fillers occurs due to a change in the rigidity of the polymer-filler system. An increase in hardness with a small amount of filler is due to a change in the degree of structural ordering of polypropylene, and a decrease in the hardness of a composition with a further increase in the content of fillers is apparently because shear deformation destroys the structures of their fillers, which, moreover, however, is not capable of active interaction with the polymer.

Therefore, upon deformation, the contacts between the filler particles are easily destroyed, and in the absence of their interaction with the polymer matrix, the entire system is weakened.

A decrease in the impact strength of CPPMs is obviously explained by the fact that an increase in the filler content leads to the appearance of large internal stresses that reduce the strength of bonds between the polymer matrix and filler particles, the appearance of dangerous defects in the form of microcracks, pores, etc.

Thus, the analysis of experimental data shows that the nature and structure of fillers has a definite effect on the physico-mechanical properties of composite materials based on polypropylene. At the same time, the fibrous-filled compositions have the greatest mechanical strength.

Figures 5-8 show the results of a study of the tribological properties of the investigated CPPM with raw cotton, depending on the nature and content of various fillers.
Fig. 5. Dependences of the coefficient of friction of CPPM with raw cotton (P=0,02 MPa, V=2 m/s, W=8,2%) on the type and content of fillers.

As seen from Fig. 5, with the introduction of graphite, soot, kaolin, talc and wollastonite into the composition of polypropylene, a decrease in the coefficient of friction of the polypropylene composition with raw cotton is observed. The introduction of the remaining fillers causes an increase in the coefficient of friction. Also, due to the high viscosity of the melt of the polypropylene composition, the critical values of the content of the filler are reduced. So, for example, the minimum coefficient of a polypropylene composition is observed at 15-20 m.p. including graphite and soot. With an increase in the content of fiberglass, cotton lint, chalk, wollastonite, talc and kaolin, the coefficient of friction of composite polyethylene materials with raw cotton increases.

A decrease in the coefficient of friction of CPPM filled with talc and kaolin is associated with their lamellar structure and fine dispersion. Composite materials filled with soot and graphite have a relatively low thermal conductivity.

An increase in the coefficient of friction of composite materials with raw cotton at high filler contents is associated with an increase in their surface roughness due to aggregation of the filler and a decrease in the physical and mechanical properties of the material due to insufficient wetting of the filler particles by the polymer matrix.

Analysis of the results of studying the change in the intensity of linear wear of composite polypropylene materials during friction with raw cotton, depending on the content of the filler (Fig. 6), shows that with an increase in the content of talc and kaolin to 10-20 m.p. the wear rate remains almost unchanged, despite a slight increase in the friction coefficient (Fig. 5). The introduction of graphite and soot increases the wear rate, which correlates with a change in the coefficient of friction. An increase in the wear rate of composite materials with an increase in the content of soot and graphite is explained by a decrease in the hardness and embrittlement of the material.

In addition, with an increase in the content of fiberglass, wollastonite, cement and kaolin, the wear rate of composite materials first decreases, then, after passing through a minimum, it increases. Moreover, the minimum and its value, depending on the content and nature of the filler, are different.

Composite polymer materials filled with wollastonite, cotton lint and fiberglass are highly resistant to wear. For materials filled with fiberglass and cotton lint, the wear rate...
decreases to a minimum value and the friction coefficient increases with an increase in their content.

As a result of the studies carried out, fillers were established, with an increase in the content of which the coefficient of friction and the intensity of wear of the composition during friction with raw cotton were reduced.

![Dependence of linear wear rate of CPPM with raw cotton on filler type and content](image1)

**Fig. 6.** Dependences of the linear wear rate of CPPM with raw cotton (P=0.02 MPa, V=2 m/s, W=8.2%) on the type and content of fillers.

It was found that the following filler contents are optimal for the minimum friction coefficient of CPPM: soot and graphite 5-25 m.p., talc 10-30 m.p., kaolin 10-30 m.p., chalk 10-40 m.p.

For the minimum value of the wear rate of composite polymer materials during rubbing with raw cotton, the optimal filler content for polypropylene and polyethylene compositions is 5-30 m.p. including fiberglass and chalk, 5-25 m.p. including kaolin and talc.

The study of the friction coefficient and the wear rate of composite polymer materials does not make it possible to explain the interaction process in the polymer-cotton system without the results of studying the temperature and static electricity charge in the friction zone, which can lead to undesirable phenomena, such as a decrease in the performance of machines, a fire, etc.

In this regard, research has been carried out to study the appearance of temperature and static electricity in the friction zone.

As seen from Fig. 7, a polypropylene composition by friction with raw cotton, with the introduction of fillers of graphite, soot and wollastonite, the temperature in the friction zone decreases, and with the introduction of fillers of cotton lint, fiberglass, talc and kaolin, an increase in temperature is observed.
As a result of the studies carried out, fillers were established, with an increase in the content of which the coefficient of friction and the intensity of wear of the composition during friction with raw cotton were reduced.

**Fig. 6.** Dependences of the linear wear rate of CPPM with raw cotton (P=0.02 MPa, V=2 m/s, W=8.2%) on the type and content of fillers.

It was found that the following filler contents are optimal for the minimum friction coefficient of CPPM: soot and graphite 5-25 m.p., talc 10-30 m.p., kaolin 10-30 m.p., chalk 10-40 m.p.

For the minimum value of the wear rate of composite polymer materials during rubbing with raw cotton, the optimal filler content for polypropylene and polyethylene compositions is 5-30 m.p. including fiberglass and chalk, 5-25 m.p. including kaolin and talc.

The study of the friction coefficient and the wear rate of composite polymer materials does not make it possible to explain the interaction process in the polymer-cotton system without the results of studying the temperature and static electricity charge in the friction zone, which can lead to undesirable phenomena, such as a decrease in the performance of machines, a fire, etc.

In this regard, research has been carried out to study the appearance of temperature and static electricity in the friction zone.

As seen from **Fig. 7**, a polypropylene composition by friction with raw cotton, with the introduction of fillers of graphite, soot and wollastonite, the temperature in the friction zone decreases, and with the introduction of fillers of cotton lint, fiberglass, talc and kaolin, an increase in temperature is observed.

**Fig. 7.** Dependences of temperature in the friction zone of CPPM with raw cotton (P=0.02 MPa, V=2 m/s, W=8.2%) of the type and content of fillers.

From the results of experimental studies (Figure 8) it can be seen that in the process of friction, electric charges arise and accumulate. As a result, the tension and electric forces in the double electric layer increase, which possibly, leads to an increase in the total frictional force.

**Fig. 8.** Dependences of the magnitude of the charge of static electricity during friction of CPPM with raw cotton (P=0.02 MPa, V=2 m/s, W=8.2%) of the type and content of fillers.
With an increase in the content of talc and kaolin in polypropylene composites, the degree of their electrification increases, the value of charges at 40 m.p. is equal to $31.5 \times 10^{-7}$ and $35.6 \times 10^{-7}$ C, $26.7 \times 10^{-7}$ and $31.3 \times 10^{-7}$ C, respectively. This is explained, apparently, by the fact that talc significantly improves the electrical insulating properties of the compositions.

Filling the composition with graphite and soot causes a strong decrease in the static electricity charge when rubbed with raw cotton.

The addition of talc, kaolin, fiberglass, cotton lint, chalk to the polypropylene composition increases the amount of charge, while the addition of graphite, soot and wollastonite decreases it. This is due to the different effect of mineral fillers on the electrical conductivity of polymer compositions. With an increase in the content of mineral fillers of conductors and semiconductors, the number of contacts between particles increases, and the surface of the contacts increases. As a result, the electrical and thermal conductivity of composite polymer materials increases. An increase in the content of talc and kaolin also causes an increase in contacts between filler particles, but this leads to a slight increase in electrical resistance and a decrease in the thermal conductivity of composite material.

Filling polypropylene compositions with wollastonite causes a decrease in the amount of static electricity when rubbed with raw cotton. Wollastonite, having a higher electrical conductivity than other fillers, somewhat reduces electrification, which is associated with a higher conductivity and charge leakage in composite polymer materials filled with wollastonite.

4 Conclusions

It has been shown that the physical, mechanical and strength properties, as well as the coefficient of friction, the rate of wear, the magnitude of the charge of static electricity, and the temperature in the friction zone of CPPM with raw cotton, depend on the type, nature and content of fillers.

It has been established that the introduction of carbon-graphite fillers into the composition of structural CPPM leads to a significant increase in the physical, mechanical and strength properties, a decrease in the friction coefficient, temperature and the magnitude of the static electricity charge in the friction zone with raw cotton.

The introduction of mineral fillers significantly increases their strength properties, the coefficient of friction of the CPPM with raw cotton, the temperature and the amount of static electricity in the friction zone, and at the same time reduces the wear rate of the composite material. An exception is a composite polymer material with fillers such as talc and kaolin, which have a plate-like structure and reduce the coefficient of friction polymer composite.

The efficiency of decreasing the wear rate and increasing the strength properties of CPPM increases with the introduction of fillers of a fibrous type, which provide high strength and resistance of the material to thermal effects.

The established regularities of changes in the properties of structural CPPM during frictional interaction with raw cotton on the type and content of fillers are consistent with the molecular-mechanical-electrical theory of friction, based on which it is possible to develop promising structural composite materials for operation in conditions of contact interaction with raw cotton allowing the manufacture of parts of the working bodies of machines and mechanisms.
increases, and the surface of the contacts increases. As a result, the electrical and thermal fillers of conductors and semiconductors, the number of contacts between particles composition increases the amount of charge, while the addition of graphite, soot and composite material. A slight increase in electrical resistance and a decrease in the thermal conductivity of and kaolin also causes an increase in contacts between filler particles, but this leads to a conductivity of composite polymer materials increases. An increase in the content of talc wollastonite.

conductivity than other fillers, somewhat reduces electrification, which is associated with a of static electricity when rubbed with raw cotton. Wollastonite, having a higher electrical electricity charge when rubbed with raw cotton.

Compositions, the fact that talc significantly improves the electrical insulating properties of the CPPM increases with the introduction of fillers of a fibrous type, which provide high composite. An exception is a composite polymer material with fillers such as talc frictional interaction with raw cotton on the type and content of fillers are consistent with machines and mechanisms.

In filling polypropylene compositions with wollastonite causes a decrease in the amount Filling the composition with graphite and soot causes a strong decrease in the static coefficient of friction, the rate of wear, the magnitude of the charge of static electricity, and magnitude of the static electricity charge in the friction zone with raw cotton. It has been shown that the physical, mechanical and strength properties, as well as the degree of electrification increases, the value of charges at 40 m.p. is equal to 31,5 \cdot 10^{-7} C, 26,7 \cdot 10^{-7} C, respectively. This is explained, apparently, by


