

Effect of Monoethanolamine Concentration on CO₂ Removal using Continuous High Frequency Ultrasonic Reactor

Siti Munirah Mhd Yusof¹, Azmi Mohd Sharif^{1,}, Tay Wee Horng¹, Farhana Ajua Mustafa¹, Lau Kok Keong¹*

¹ CO₂ Research Centre (CO₂RES), Department of Chemical Engineering, Universiti Teknologi PETRONAS, Bandar Seri Iskandar, 32610, Perak, Malaysia

Chemical absorption is the most common technology used for the process of CO₂ removal from natural gas due to its ability to reduce the level of the acid gas to a very low level as well as higher mass transfer performance due to the chemical kinetic reaction. Higher solvent concentration resulted in higher capacity to remove CO₂, however reduces the diffusivity as well as its ability to spread on the packing due to its high solvent viscosity. This has hindered the used of high viscosity solvent in the operation of conventional packed column. However, recent technology of using high frequency ultrasonic irradiation for absorption process has shown possibility to operate high viscosity solvent due to the absence of packing in the reactor. From this work, it is shown that high viscosity solvent does not affect the mass transfer performance under ultrasonic irradiation due to the presence of acoustic streaming, fountain and atomization that reduced the film resistance thus increases the diffusivity. This work has demonstrated that this technology has high flexibility of solvent selection for the absorption process.

1 Introduction

In the chemical absorption process, CO₂ gas is removed from natural gas by reacting with chemical solvent and form intermediate compounds. Chemical absorption is mainly used in the separation process because it can reduce the level of acid gas to a very low level. There are a number of solvents that have been used for the chemical absorption of CO₂ such as amines, ammonia and potassium carbonate [1-7]. Among those solvents, amines especially monoethanolamine (MEA) is the most well-developed and commonly used for CO₂ removal from gas streams such as sour natural gas [2, 8, 9].

Other than having higher reactivity than secondary and tertiary amine, MEA also exhibited higher mass transfer performance than ammonia [1, 5]. Besides, MEA is also used for the absorption process due to its high absorption capacity and low cost [10, 11]. Higher MEA concentration provides higher amount of active MEA in the bulk solvent thus increasing the mass transfer performance. However, the increase in MEA concentration resulted in the increase of the solvent viscosity. This affects the mass transfer performance of the absorption process due to slower diffusion of amine from the bulk solvent to the gas-liquid interfacial area and also slower diffusion of the gas to the reactive boundary layer. Furthermore, for packed column operation, the use of high viscosity solvent resulted in decrease of absorption performance due to the reduced in turbulence on the packing surface as well as lower solvent ability to spread on the packing [12, 13]. In addition, high viscosity solvent caused operational issue

for packed column operation [14]. Thus, the operation of the packed column for high viscosity solvent is less feasible.

Recently, a new technology of using high frequency ultrasonic irradiation has shown higher CO₂ absorption performance as compared to the packed column [4, 15-17]. This technology successfully enhanced the mass transfer process due to the physical effects of ultrasonic irradiation that increases the gas-liquid interfacial area without having any packing in the column. Due to the absence of the packing, the use of high viscosity solvent for the absorption process might be possible. Therefore, in this work, the effect of MEA concentration on the mass transfer performance of CO₂ absorption using high frequency ultrasonic irradiation in a continuous system is reported.

2 Experimental Procedure

2.1. Chemical and Materials

MEA used in the experiment is of 99% purity purchased from MERCK. CO₂ gas purchased from Air Products is of 99% purity. The natural gas (NG) purchased from Petronas Dagangan Bhd. is of 97% purity.

2.2 Experimental Set Up and Operation

The detailed experimental set up and operation has been described in our previous work [17]. The high frequency ultrasonic reactor used in this study consists of 4 unit of

* Corresponding author: azmish@utp.edu.my

ultrasonic transducers and no packing. Table 1 shows the constant process parameters in this work. The MEA concentration was varied at 30 wt.% and 70 wt.%.

Table 1 Constant operating parameters

Parameter	Value
CO ₂ concentration (%)	20
Pressure (bar)	50
Temperature (°C)	30
Ultrasonic Frequency (MHz)	1.7
Ultrasonic Power (W)	33

2.3 Overall Volumetric Mass Transfer Coefficient

The overall volumetric mass transfer coefficient calculation followed the work done by A. Setameteekul et al.(2008) as expressed in Eq. (1) and Eq. (2) [12].

$$K_G a_v = \frac{\dot{n}_{CO_2}}{\Delta P_{1,M}} \quad (1)$$

Where

$$\Delta P_{LM} = P \left[\frac{(y_{CO_2,G} - y^*_{CO_2,G})_{in} - (y_{CO_2,G} - y^*_{CO_2,G})_{out}}{\ln \frac{(y_{CO_2,G} - y^*_{CO_2,G})_{in}}{(y_{CO_2,G} - y^*_{CO_2,G})_{out}}} \right] \quad (2)$$

where \dot{n}_{CO_2} is the absorption rate in mol/m³.hr; P is the total pressure of the system in kPa; $Y_{CO_2,in}$ and $Y_{CO_2,out}$ are the CO₂ concentration in the gas entering and leaving the absorber respectively; $y_{CO_2,G}$ is the CO₂ mole fraction in the gas phase while $y^*_{CO_2,G}$ is the equilibrium mole fraction. A log mean driving force was used since the liquid phase is assumed to be well-mixed due to the ultrasonic acoustic streaming and the gas phase is assumed as plug flow since the composition changes significantly from inlet to outlet.

2.3 Physical Properties of MEA

The viscosity of the solvent was obtained based on the study reported by Arachchige et al. (2013) while the diffusivity was acquired based on the work reported by Versteeg et al. (1988) [18, 19].

3 RESULTS AND DISCUSSION

Table 2 and Table 3 present the viscosity and diffusivity of 30 wt.% and 70 wt.% MEA. As shown in tables, increased in MEA concentration from 30 wt.% to 70 wt.% resulted in significant increase of the viscosity and reduction of the chemical diffusivity. The high solvent viscosity resulted in the lower liquid flow rate and low mixing effect. In addition, lower diffusivity resulted in lower mass transfer in the liquid phase.

Table 2 Viscosity of MEA solvent

MEA Concentration (wt.%)	Viscosity (mPa.s)
30	2.48
70	12.46

Table 3 Diffusivity of MEA solvent

MEA Concentration (wt.%)	Diffusivity (x10 ⁻⁹ m ² .s ⁻¹)
30	1.39
70	0.60

Figure 1 shows the effect of MEA concentration on the mass transfer coefficient. As shown in the figure, higher MEA concentration resulted in higher mass transfer performance.

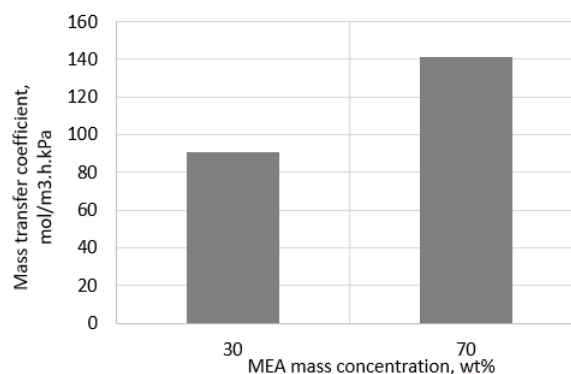


Figure 1 Effect of MEA concentration on mass transfer coefficient

This is due to the higher capacity of active MEA in the solution to remove the CO₂ from the gas stream [9, 12]. The increase of MEA concentration from 30 wt.% to 70 wt.% resulted in increased of mass transfer coefficient from 90.6 mol/m³.kPa.hr to 141.4 mol/m³.kPa.hr. In the study done by Setameteekul et al.(2008), the increase in MEA concentration at low temperature of 30°C resulted in low increment of mass transfer coefficient, which is due to low spreading ability in the packing surface [12]. Due to this, low MEA concentration of 30 wt.% has been used in most of the studies conducted on CO₂ absorption in a packed column [1, 6, 8].

Even though higher MEA concentration has higher active MEA to capture the CO₂, the increase in viscosity and lower diffusion coefficient resulted in lower mass transfer increment and increase the operating difficulty of the packed column. However, from this work, it has been proved that the high viscosity does not affect the mass transfer performance under ultrasonic irradiation. This is due to the presence of high frequency ultrasonic irradiation, which generates acoustic streaming, fountain and atomization which reduces the film resistance through the mixing effect, thus increase the diffusivity. Furthermore, internal design of the reactor is empty,

unlike the conventional packed column, which is filled with packing that limits the usage of high viscosity solvent.

4 CONCLUSION

This work has shown that the increase in solvent viscosity does not affect the mass transfer performance of the absorption process using the high frequency ultrasonic irradiation system. Therefore, this technology has great potential for the enhancement of absorption technology since it can provide higher mass transfer performance as well as higher flexibility of solvent selection as compared to the conventional packed column.

Acknowledgement

Research supports were provided by CO₂ Research Center (CO2RES), Universiti Teknologi PETRONAS.

References

- [1] G. Puxty, R. Rowland, and M. Attalla, "Comparison of the rate of CO₂ absorption into aqueous ammonia and monoethanolamine," *Chemical Engineering Science*, vol. 65, pp. 915-922, 2010.
- [2] M. Afkhamipour and M. Mofarahi, "Review on the mass transfer performance of CO₂ absorption by amine-based solvents in low-and high-pressure absorption packed columns," *RSC Advances*, vol. 7, pp. 17857-17872, 2017.
- [3] P. Luis, "Use of monoethanolamine (MEA) for CO₂ capture in a global scenario: Consequences and alternatives," *Desalination*, vol. 380, pp. 93-99, 2016.
- [4] W. H. Tay, K. K. Lau, and A. M. Shariff, "High performance promoter-free CO₂ absorption using potassium carbonate solution in an ultrasonic irradiation system," *Journal of CO₂ Utilization*, vol. 21, pp. 383-394, 2017/10/01/ 2017.
- [5] C.-H. Yu, C.-H. Huang, and C.-S. Tan, "A review of CO₂ capture by absorption and adsorption," *Aerosol Air Qual. Res.*, vol. 12, pp. 745-769, 2012.
- [6] H. Dang and G. T. Rochelle, "CO₂ absorption rate and solubility in monoethanolamine/piperazine/water," *Separation science and technology*, vol. 38, pp. 337-357, 2003.
- [7] B. Jafari, M. R. Rahimi, M. Ghaedi, K. Dashtian, and S. Mosleh, "CO₂ capture by amine-based aqueous solution containing atorvastatin functionalized mesocellular silica foam in a counter-current rotating packed bed: Central composite design modeling," *Chemical Engineering Research and Design*, vol. 129, pp. 64-74, 2018.
- [8] S. Freguia and G. T. Rochelle, "Modeling of CO₂ capture by aqueous monoethanolamine," *AIChE Journal*, vol. 49, pp. 1676-1686, 2003.
- [9] H. N. Abdul Halim, A. M. Shariff, L. S. Tan, and M. A. Bustam, "Mass transfer performance of CO₂ absorption from natural gas using monoethanolamine (MEA) in high pressure operations," *Industrial & Engineering Chemistry Research*, vol. 54, pp. 1675-1680, 2015.
- [10] Y. Chunbo, C. Guangwen, and Y. Quan, "Process characteristics of CO₂ absorption by aqueous monoethanolamine in a microchannel reactor," *Chinese Journal of Chemical Engineering*, vol. 20, pp. 111-119, 2012.
- [11] M. H. El-Naas, Z. M. Ismail, and M. H. Al-Marzouqi, "Correlating the physical solubility of CO₂ in several amines to the concentrations of amine groups," *Journal of Natural Gas Science and Engineering*, vol. 34, pp. 841-848, 2016.
- [12] A. Setameteekul, A. Aroonwilas, and A. Veawab, "Statistical factorial design analysis for parametric interaction and empirical correlations of CO₂ absorption performance in MEA and blended MEA/MDEA processes," *Separation and Purification Technology*, vol. 64, pp. 16-25, 2008/11/20/ 2008.
- [13] D. Song, A. F. Seibert, and G. T. Rochelle, "Mass transfer parameters for packings: effect of viscosity," *Industrial & Engineering Chemistry Research*, vol. 57, pp. 718-729, 2018.
- [14] L. Tan, A. Shariff, K. Lau, and M. Bustam, "Factors affecting CO₂ absorption efficiency in packed column: a review," *Journal of Industrial and Engineering Chemistry*, vol. 18, pp. 1874-1883, 2012.
- [15] W. Tay, K. Lau, and A. Shariff, "High frequency ultrasonic-assisted CO₂ absorption in a high pressure water batch system," *Ultrasonics sonochemistry*, vol. 33, pp. 190-196, 2016.
- [16] W. Tay, K. Lau, and A. Shariff, "High frequency ultrasonic-assisted chemical absorption of CO₂ using monoethanolamine (MEA)," *Separation and Purification Technology*, vol. 183, pp. 136-144, 2017.
- [17] S. M. M. Yusof, K. K. Lau, A. M. Shariff, W. H. Tay, N. F. A. Mustafa, and S. S. M. Lock, "Novel continuous ultrasonic contactor system for CO₂ absorption: Parametric and optimization study," *Journal of Industrial and Engineering Chemistry*, 2019.
- [18] U. Arachchige, N. Aryal, D. A. Eimer, and M. C. Melaaen, "Viscosities of pure and aqueous solutions of monoethanolamine (MEA), diethanolamine (DEA) and N-methyldiethanolamine (MDEA)," *Annual Transactions of the Nordic Rheology Society*, vol. 21, p. 299, 2013.
- [19] G. F. Versteeg and W. P. Van Swaaij, "Solubility and diffusivity of acid gases (carbon dioxide, nitrous oxide) in aqueous alkanolamine solutions," *Journal of Chemical & Engineering Data*, vol. 33, pp. 29-34, 1988.