Imparting hydrophobic functionalities to copper surface using laser ablation and water emulsion of surfactants

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Abstract. Wettability is one of the main characteristics of a surface and reflects the ability of a liquid to flow over a solid surface. Using hydrophobic functional surfaces in evaporator and condenser of heating plants to intensify heat exchange processes will increase efficiency and, consequently, reduce the metal consumption and weight-size parameters of this equipment. This will result in reduced energy consumption and lower production and operating costs. This paper presents an analysis of methods for creating hydrophobic surfaces. The fabrication of hydrophobic copper surface of experimental samples by creating multimodal relief in form of 50 μm grid by laser ablation process and subsequent reduction of surface energy of material using water emulsion of octadecylamine is grounded and described. The fluence was varied from 5 to 900 J/cm^2 when modifying the surface using laser station. The dependence of the effect of laser fluence on water contact angle value is presented. Following the study, the optimum laser irradiation parameters for the surface of experimental samples were determined, at which the maximum value of water contact angle of 146.61° and the minimum value of roll-off angle of 13.5° were obtained.

1 Introduction

One of the strategic objectives in the energy industry is to improve the reliability and efficiency of heat exchange equipment in heating plants. Thus, phase-change apparatuses (in which the heat transfer agent boils or condenses) are widely used in various heating equipment not only in traditional power engineering, but also in the use of renewable energy sources (RES).

Heat pumps, refrigeration machines and turbines based on low boiling point fluids (LBPF) are widely used in the RES-based energy supply of consumers. Such equipment uses an evaporator and condenser as the main heat exchangers, which are highly metal consuming and have considerable weight-size parameters (Fig. 1). Intensification of heat exchange processes in evaporator and condenser will allow to increase efficiency and, as a consequence, to reduce metal consumption, weight and dimensions of this heat exchangers.

Fig. 1. ORC unit by TURBODEN [1].

The current approach is to use porous coatings, finning, knurling, dimpled surfaces, inclined surfaces, etc. to intensify the heat transfer during boiling and condensation [2].

Analysis of various studies shows that the most promising way of intensification of boiling and condensation processes is the use of hydrophobic functional surfaces. Thus, research work [3] studied free convection and heat transfer of evaporating droplets on initial and hydrophobic substrate made of aluminium-magnesium alloy AlMg6. The surface of the experimental sample was made hydrophobic by laser ablation process followed by coating with nanofluid (aqueous solution of SiO_2 silicon dioxide), resulting in a water contact angle of $155\text{--}160^\circ$. The study determined

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that the heat transfer coefficient for the hydrophobic surface is 25-30% higher than for the initial substrate.

The authors of [4] have developed a fast and simple process for fabrication of silicon based thin film coating. This technique makes it possible to achieve a hydrophobic surface state. In this case the value of the water contact angle is 105 degrees. Experimental studies were carried out on a water vapour condensation unit. Fig. 2 shows the schematic diagram of this unit. The experimental results indicated that the said silicon coating on copper tube surface, as compared to untreated copper tube, contributes to increase the heat transfer coefficient during condensation by 50%. It was also observed that the addition of silicon oil to synthetic film can significantly increase the evaporation rate of water droplets from the surface, while the surface wettability remains the same.

Fig. 2. Schematic view of water vapour condensation plant [5].

In research work [5] a comparative analysis of heat transfer coefficient values in vertical plate heat exchangers made of brass 464 in the initial state and with PTFE-based hydrophobic coating was carried out. Analysis of the results of experiments carried out at identical operating parameters indicates that the use of hydrophobic coatings contributes to increase in the heat transfer coefficient by 4 times, compared with the surface in the initial state.

In addition, hydrophobic surfaces contribute to reducing the rate of deposit formation and corrosion processes [6].

The scientific community has identified the basic conditions that must be met in order to create superhydrophobic surfaces [7]:

- creation of multimodal relief on the surface of material;
- reducing the surface energy of the solid surface of material.

There are many ways to create hydrophobic metal surfaces. Electrodeposition of nanoparticles, chemical vapour deposition and etching, plasma treatment, etc. are the most common. These methods are very expensive, complicated and have low mechanical properties of the treated surface structure. For example, hydrophobic surfaces made using some of the above-

mentioned techniques are very brittle and the coating may delaminate [8].

The modification of surfaces of various construction materials using laser equipment is currently being actively developed. This method does not have any of the previously mentioned disadvantages and allows the creation of a multimodal ordered topography with repeatable geometric characteristics. This makes it possible to achieve high values of the water contact angle. However, the construction material surface after the laser ablation process has hydrophilic properties due to formation of metal oxides on it [9].

Surface energy can be reduced by storing the laser-modified sample in the air for 10-30 days [10-12] (Fig. 3), by creating a surfactant layer on its surface [8] and by other ways.

Fig. 3. Images of water droplet shape on modified surface on day 1 (a), day 7 (b) and day 20 (c) after laser ablation processing.

The duration of imparting hydrophobic properties to the surface when stored in ambient air is one of the reasons preventing mass production for industrial applications. It should be noted that the layer formed by adsorption of airborne organic compounds on laser-treated surface is easily removed from surface by exposure to liquid media. As a consequence, there is deterioration in the non-wettability properties of the surface [14].

The authors of [12] used 50x50 mm mirror-polished stainless steel 316L plates as experimental samples. Imparting hydrophobic functionalities to metal surface was carried out using 1030 nm laser equipment with the following source parameters: scan speed was 100 mm/s, rep rate was 100 kHz and pulse duration was 10 picoseconds. The value of water contact angle, which increased between 77 and 154 degrees, was measured after exposing the samples to ambient air for 30 days in order to sorb the organic substances on their surface.

In research work [15], experimental samples made of aluminium AA2024 were coated with a perfluoropolyether compound as a hydrophobic agent after laser texturing of the surface. The sample surface in the initial state demonstrated hydrophilic properties and the value of the water contact angle was $59 \pm 2^\circ$. After surface modification, the water contact angle was $166 \pm 2^\circ$.

In the present study, imparting hydrophobic functionalities to the copper surface of experimental samples was performed by using a laser station to fabricate a grid pattern with lines equidistant by 50 μm , followed by formation of surfactant layers. The influence of laser fluence on surface wettability properties of the samples was analysed.

2 Description of research methods

To study the change of functional surface, plates with dimensions 40x40 mm and thickness of 1 mm made of flat copper M1t were used as experimental samples.

After the copper plates were made, the surface was cleaned of various contaminants using ethyl alcohol and then washed with distilled water to remove solvent residues.

The multimodal relief was formed on the surface of experimental samples using the FMark-20 NS-FB laser station (Fig. 4) with the following technical specifications:

- 1064 nm ytterbium fibre laser;
- rep rate ranges from 20 to 100 kHz;
- maximum output power is 20 W;
- scan speed up to 10 m/s;
- pulse duration ranges from 4 to 200 ns;
- spot size is 59 μm .

The laser beam is focused on the treated surface using MS-II-10 dual axis deflection system (RAYLASE AG, Germany). Linos lens with focal length of 163 mm and scan field of 110x110 mm was used for laser scanning.

Fig. 4. Photo: Laser station FMark-20 NS-FB.

To produce a gridded relief structure, the laser beam moved along the sample surface along mutually perpendicular lines spaced at equal distance of 50 μm from each other. During the treatment of experimental samples surfaces the laser fluence was varied in the range from 5 to 900 J/cm², which corresponds to the following parameters: laser output power was 12, 20 W, rep rate was 20, 100 kHz, and scan speed varied in the range from 42 to 5555 mm/s. Laser radiation parameters for each of experimental samples are presented in Table 1.

Table 1. Laser fluence for each experimental sample.

Sample No.	Laser output power, W	Rep rate, kHz	Scan speed, mm/s	Laser fluence, J/cm ²
1	12	20	5555,1	5
2	12	20	2340,9	10
3	12	20	914,9	25
4	20	20	835,7	50
5	20	20	386,7	100
6	20	20	255,1	150
7	20	20	190,7	200
8	20	20	152,3	250
9	20	20	126,8	300
10	20	20	108,6	350
11	20	20	95,0	400
12	20	20	84,5	450
13	20	20	76,0	500
14	20	20	63,3	600
15	20	20	54,3	700
16	20	20	47,5	800
17	20	20	42,2	900

Molecular surfactant layers were formed on the surface of textured samples using a designed and

constructed unit. Fig. 5 shows the schematic diagram of this unit.

Fig. 5. Schematic diagram of unit for formation of molecular layers of surfactants on surface of experimental samples.

This unit consists of a laboratory heated bath (3) with electric heating of liquid (7), in which a glass container (2) is immersed to form molecular layers of surfactant, as which octadecylamine (ODA) was used. At the bottom of container the experimental samples (5) are evenly placed in horizontal position, then paddle (4) is immersed and rotated planetary and multidirectionally by rotating device (1), thus providing uniform mixing of ODA emulsion (6).

In the experiment, a bath is heated by means of electric heating elements, then a container filled with 3 L of distilled water is immersed in the heated bath. When the water temperature in container reaches 80 °C [16], 9 mg of octadecylamine is added and actively stirred to a homogeneous emulsion using rotating device. The experimental samples are then lowered to the bottom of container with emulsion and the mixing paddle is immersed. The paddle is rotated both about its own axis and about the axis of the glass container, coaxial to rotating device, for 30 minutes. After this time, the samples are removed from emulsion and air dried for 24 hours until the treated surface is completely dry. Fig. 6 shows images of surface of experimental samples in their initial state and after modification using the laser station and aqueous emulsion of ODA.

Fig. 6. Images of experimental samples with initial (a) and modified surface at laser fluence of 50 (b), 250 (c) и 900 (d) J/cm².

Fig. 6 (b - d) shows that the experimental samples after laser ablation and formation of molecular layers of ODA have colour differences. This is primarily due to the fact that the geometric characteristics of relief, such as side protrusion height and channel depth, increases as the laser fluence increases.

After the modified sample surface had completely dried, the values of water contact angle and roll-off angle were determined using an OCA 20 device (Fig. 7) (enters as part of large-scale research facilities «Hydroshock test rig Erosion-M») and 5 and 30 µl drops of distilled water, respectively (Fig. 8). Water contact angle and roll-off angle were measured on three different areas of the experimental sample surface modified with laser station and ODA aqueous emulsion to improve the accuracy of the results obtained. The average value of water contact angle and roll-off angle was then calculated.

Fig. 7. Photo: OCA 20 device for measuring water contact angle and roll-off angle.

Fig. 8. Photo: Measuring water contact angle (a) and roll-off angle (b).

The surface of experimental samples in their initial state and after relief formation was also examined using SEM Tescan MIRA 3 (Fig. 9). Fig. 9 demonstrates that the laser ablation process has fabricated multimodal ordered microrelief with repeatable geometric characteristics.

Fig. 9. Images of initial state (a), modified state (b) and micrographic specimen (c) of copper surface.

Fig. 10. Dependence of water contact angle on laser fluence.

Fig. 10 shows that increasing in laser fluence from 0 to 300 J/cm² leads to an increase in the water contact angle. However, a further increase in the laser fluence leads to a decrease in the water contact angles.

The maximum value of the water contact angle of 146,61° was obtained at a laser fluence of 300 J/cm². The value of the roll-off angle for this surface is 13.5°. This value is the minimum for the experimental samples considered.

Conclusions

In this work, a grid pattern with lines equidistant by 50 μm was created on the copper sample surface using a laser station, followed by the formation of ODA layers to reduce the surface energy of material.

3 Results obtained

The copper surface in its initial state demonstrates hydrophilic properties and the values of the water contact angle and roll-off angle are 70.16° and 77.53°, respectively. Immediately after laser texturing, all experimental samples achieve a hydrophilic surface state. The modification of the experimental samples using laser ablation process and ODA aqueous emulsion resulted in all surfaces becoming hydrophobic and water contact angle ranging from 102.9 to 146.6 degrees.

The effect of laser fluence on water contact angle was studied (Fig. 10). A surface modified solely with octadecylamine aqueous emulsion at similar parameters was chosen as the initial point at which the laser fluence was zero. The value of the water contact angle for this surface was 104°.

Analysis of effect of laser fluence on water contact angle (Fig. 10) indicates that the maximum values of water contact angle are reached at 250, 300 J/cm².

The surface of experimental sample No. 9 (Table 1) with a minimum roll-off angle of 13.5° and maximum water contact angle of 146.61° was obtained at laser fluence of 300 J/cm².

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