Deformation behavior of Austenitic stainless steel at subzero temperature

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Abstract Austenitic stainless steel is one of the second generation advanced high strength steel which finds application in automobile, aerospace and cryogenic components. The component made of austenitic steel might operate in subzero temperature condition because of its excellent formability even at subzero temperature. In the present work several tensile tests were performed on austenitic stainless-steel sheet of thickness 1.2 mm at 0°C, -40°C, -80°C, -120°C and at different strain rates of 0.01/sec, 0.001/sec, 0.0001/sec. The resultant mechanical properties, like yield strength, tensile strength, elongation percent and strain hardening exponent, along with phase fractions and microstructural properties were analyzed to understand the reasons for change in mechanical properties, on comparing with room temperature properties. It was noticed that tensile strength is 635 Mpa, & strain hardening exponent is 0.38 at room temperature (25 °C) and tensile strength is 1236 Mpa, & strain hardening exponent is 0.49 at -120°C. Similarly, XRD characterization revealed that strain induced martensite increased from zero percent at 25°C (room temperature) to 57 percent at-120°C. Similarly EBSD characterization revealed that grain average misorientation which also increased from room temperature to-120°C.

Keywords Subzero temperature, Austenitic stainless steel, strain rates, phase fractions, XRD characterization, EBSD characterization, mechanical properties.

1.Introduction

Stainless steels are basically alloys of Iron (Fe), carbon(C), and chromium (Cr), exhibits excellent corrosion resistance property because of the strong, non-porous chromium oxide layer (Cr2O3) on the surface of the steel. Stainless steel [10] can be Ferritic, Austenitic, Martensitic, duplex and precipitation hardened type based on chromium and carbon percent. Usually ferritic stainless steels show BCC structure & contains low carbon in the range of 0.01t0.12 with 10.5% to 27% chromium. Martensitic stainless steels contain carbon in the range of 0.10 to 0.15% with 12% to 14% chromium. Whereas Austenitic stainless-steel show FCC structure & contains very low carbon in the range of 0.02 to 0.06% with 18% to 20% chromium along with 8% to 10% nickel. Nickel is added to stabilize Austenite phase in stainless steels [1, 2, 12]. Hence Austenitic Stainless steels are corrosion resistant and ductile than others, hence having excellent formability at room temperature, even at subzero temperature because of stable of Austenite phase. Hence these steels are best preferred for cryogenic applications. However, because of low stacking fault energy aprox 17MJ/.M2, Austenite phase transforms to Martensite on deformation. This strain induced martensite [5, 8,9] increases strength and hardness of the component. The amount of martensite formed depend on amount of deformation which can be characterized by microscopic examination and XRD characterization. Similarly grain average misorientation also increases with increase of deformation which is characterized by EBSD analysis [11].

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Swadesh et al. [4] determined tensile behaviour of SS304 at high temperature say 50°C, to 650 °C at interval of 50°C, B petit et al. [8] determined deformation behaviour of SS 304 at -60°C at various stain rates and Norimitsu koga[5] studied deformation behaviour of Duplex stainless steel. But deformation behavior of SS304 at subzero temperatures say -40°C, -80°C -120°C and at strain rates of 0.01/sec.0.001/sec,0.0001/sec is not focused much. Hence in the current study is focused much on those areas to get an insight on cryogenic behaviour of AISI304.

2 Experimentation
The material used for this work is Austenitic Stainless steel, AISI 304 of thickness 1.2mm. This material was supplied in Cold rolled & annealed condition by the local manufacturer. As received material was tested for chemical composition, mechanical properties and microstructure.

For chemical composition, sheet sample of 50mmx50 mm was cut from the sheet by using hand shear, then rough polished on 80 grid sandpaper, then chemical composition was analyzed by taking a burns on spark emitting Spectrometer Thermo Jarallesh. Chemical composition was given in table 1 similarly, for hardness value, sheet sample of 50mmx50 mm was cut from the sheet by using hand shear, and then hardness value determined by using Rockwell hardness tester with ball indenter and ‘B’ Scale. The hardness value is given in table 2. For mechanical properties, dog bone shaped sample cut, from the received sheet in the rolled direction by using water jet machining as per ASTM E08 as shown in figure 1, then tensile properties determined by using 250KN MTS axial loading system as shown in figure 2. Subzero temperature required is obtained by injecting liquid nitrogen into the chamber of testing system and necessary temperature is monitored by sensor. By using the load Vs elongation data obtained from tensile test, engineering stress, engineering strain, true stress, true strain and strain hardening exponent calculated [6,7]. Similarly samples of size 10mmx10mm, collected close to fracture of tensile deformed zone, then polished mechanically using emery papers and then polished electrolytic ally by using electrolyte (20% per chloric acid and 80% alcohol), then scans taken with a step size of 0.2 Pan analytical X-ray diffraclometer ,EBSD scans taken with a step size of 0.3 on GEMINI FE-SEM. For optical microscopy, sample of size 5mmx5mm cut from the as received sheet, then rough polished on emery papers which are coated with silicon carbide of fine grade say 600, 800, 1200 2500, then fine polished by using colloidal silica. Then etched with etchant 1:3 hydrochloric acid and nitric acid, then microstructure revealed at .1000X magnification on Zeiss optical Microscope as shown in figure 6.

<table>
<thead>
<tr>
<th>C</th>
<th>Cr</th>
<th>Ni</th>
<th>Si</th>
<th>Mn</th>
<th>P</th>
<th>S</th>
<th>Mo</th>
<th>N</th>
<th>Fe</th>
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<tbody>
<tr>
<td>0.029</td>
<td>18.66</td>
<td>8.066</td>
<td>0.33</td>
<td>1.44</td>
<td>0.038</td>
<td>0.011</td>
<td>0.12</td>
<td>0.005</td>
<td>1.301</td>
</tr>
</tbody>
</table>

**Figure:** 1 standard sample for tensile test as per ASTM E08.

<table>
<thead>
<tr>
<th>Hardness (HRB)</th>
<th>Yield strength (Mpa)</th>
<th>Tensile Strength (Mpa)</th>
<th>Strength coefficient (Gpa)</th>
<th>Elongation percent (%)</th>
<th>Strain hardening exponent (n)</th>
<th>Plastic anisotropy (R)</th>
</tr>
</thead>
<tbody>
<tr>
<td>69.9</td>
<td>259.4</td>
<td>638.9</td>
<td>1.28</td>
<td>59.48</td>
<td>0.381</td>
<td>1.06</td>
</tr>
</tbody>
</table>
3 Results and discussions

As received material supplied by local manufacturer is subjected to spark emission Spectra analysis and composition analyzed. It showed carbon percent 0.029, chromium percent 18.66 and nickel percent 8.066. Complete composition is given in table 1.

Table 1 Chemical composition

As receive sheet, tested for room temperature mechanical properties like Hardness, yield strength, Tensile strength and strain hardening exponent, anisotropy etc. It was noted that yield strength is 259.4 Mpa, Tensile strength 638.9 Mpa and Strain hardening exponent is 0.381. Complete mechanical properties given in Table 2.

Table 2 Mechanical Properties

Room temperature tensile test conducted as per ASTM E08 for two sample at a strain rate of 0.001. Then average mechanical properties of two samples considered. Its stress strain diagrams for two sample shown in figure 3.

Figure 3 Stress-strain diagrams at room temperature.

Subzero temperature tensile test was conducted by using 250 KN MTS axial loading system using liquid nitrogen medium on standard tensile sample of gauge length 80mm at strain rates of 0.01, 0.001, 0.0001 and temperatures 0°C, -40°C, -80°C, -120°C and engineering stress strain diagram plotted as shown in figure 4.
Mechanical properties like yield strength, Tensile strength calculated at each temperature and strain rate and compared. It was analyzed that yield strength is 257 Mpa at room temperature at a strain rate of 0.001/sec and it was 394 Mpa at -120 °C at a strain rate of 0.0001/sec, and tensile strength was 635 Mpa at room temperature at a strain rate of 0.001/sec and 1236 Mpa at -120 °C at a strain rate of 0.0001/sec. It was observed that both yield strength and tensile strength increased with decrease of temperature and strain rate as shown in Figure 5.

The Optical Microstructure of as received sheet is as showed fully austenitic structure. The microstructure at 1000X. is shown in figure 6.

Figure 4 engineering stress strain diagram for strain rate of 0.01 & 0.001

Figure 5 Yield strength and tensile strength comparisons as function of strain rate
XRD pattern of as received sheet showed peaks of single phase, which is 100% Austenite as shown in Figure 7.

Phase fraction at each strain rate and temperature calculated by XRD characterization. It showed that increase of martensite percentage with decrease of temperature strain rate. Martensite percent was 0, at room temperature and 57 percent at -120°C. The phase fraction at -80 and at a strain rate 0.001/sec showed 50% Austenite and 50% Martencite as shown in figure 8.

Grain average misorientation is calculated at each temperature and strain rate. It was found that it was increased with decrease of temperature and strain rate. Inverse pole figures, IPF at a strain rate of 0.001/sec at -80°C and -120°C is shown in figure 9 and 10. The Average grain size of Austenite in as received condition is 35 µm (in undeformed condition).

4. Conclusions

In this work, subzero temperature tensile behaviour of AISI 304 stainless steel was studied, then stress, strain plots were compared along with mechanical properties and phase fractions and microstructure. The following conclusions were drawn:

i. Tensile strength is increased with the decrease of temperature, strain rate due increased percentage of strain induced martensite.

ii. Strain rate and temperature have strong effect on amount of martensite formation and corresponding mechanical properties.

iii. The increase in tensile strength is non uniform, due to secondary, tertiary hardening and strain aging etc.

iv. The change in Mechanical properties is significant at -80°C compared to other temperatures.

v. The predominant deformation mechanism is Phase transformation, rather than slipping and twinning.

References